The Freerider free energy inverter

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Abstract

Speed of light is in fact dependent on medium density on which light moves through and its delay within a solid medium is not **a scatter delay effect as often believed.**

In light of this statement it is then possible to accelerate an electron in vacuum or air at relativistic speeds which are still lower than c in vacuum but yet greater than the local speed of light within a metallic collector where said electron impacts against.

If the voltage across a spark gap is high enough then said electron could briefly find itself travelling inside a metallic matrix at locally superluminar speeds, just before impacting against atoms within the collector material and slowing down to thermal status.

High electron (current) speeds within the metal amplifies magnetic field around the fast electron

at high enough levels to cause the magneculization of electrons into chains (very unstable though, they will decay almost instantaneously back to covalent type electrons), but the electromagnetic disturbance of the decelerating electron below local luminar speed upon impact with the atoms of the metallic matrix will generate non-conservative electromagnetic effects.

In this paper we propose a simple electric schematic to test this theory and measure some of these effects.

The possibility to extract free energy from the aetheric media (also referred to Zero Point Energy) has already been theorized as an hadron mechanic mechanism at play in supernova explosions, therefore high energy physic might hold the key to manipulate contact type hadronic forces and fields in such a way to allow energy to break off the aetheric substratum and collected into useful work within an otherwise isolated system.

More study and modeling are required around the formulas revolving around these possible effects and the interested reader is invited to familiarize himself with the body of work of Ruggero Santilli in the domain of Hadron mechanic.

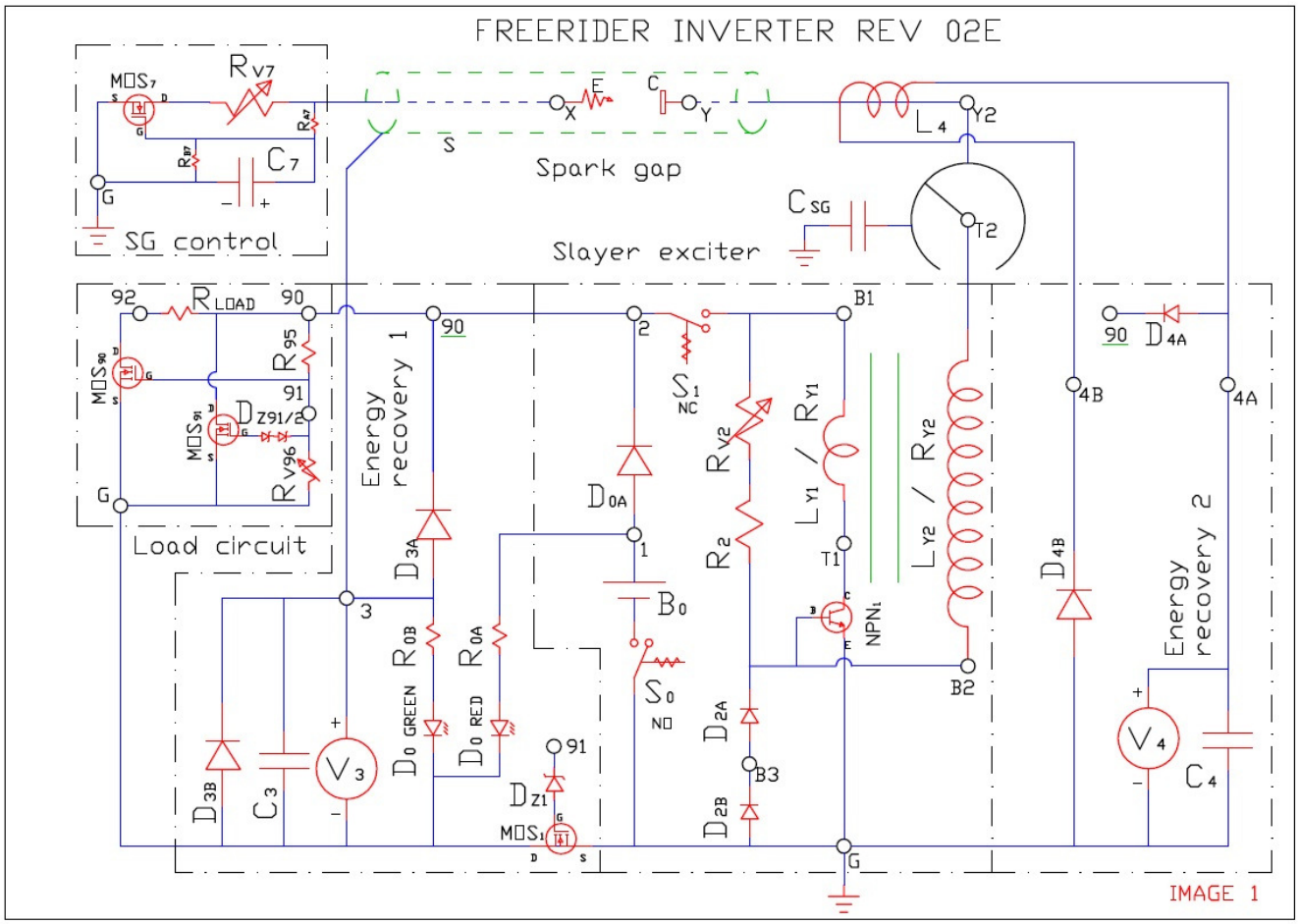
Introduction

In this paper we will present an electric machine capable of achieving overrunity energies (energy output >> energy input).

The principle of operation of this electric machine is not entirely known, but it is was inspired by Edwin Gray inverter schematics and the possible operating principle (namely overrunity power

outputs) should be found within advanced physic formula which decouple the physic forces from potential type fields (conservative type = zero energy sum = no overrunity allowed) and into hadron contact type energy forces capable of extracting net positive energy off an aetheric substrate into an otherwise isolated system (net decrease of entropy within an isolated system), which is often referred to Zero Energy Field energy.

Circuit design and operating principle



In this machine (image 1) one or more electrons are emitted from the tip of the spark gap emitter E, accelerated within the high voltage spark gap and subsequently the electron is

decelerated within the metallic matrix of the collector C.

Spark gap could be in vacuum or air with the first being the preferred method.

Collector design

The spark gap is powered by a main NPN slayer exciter or other means capable of maintaining a stable high positive voltage on the collector side during electron emission and accelerations.

The spark gap also features a thick metallic shield, this is to protect operators and personnel from harmful X-Ray radiation generated by the spark gap operations, but it is also required to collect some energy made available by the spark process.

Emitter design

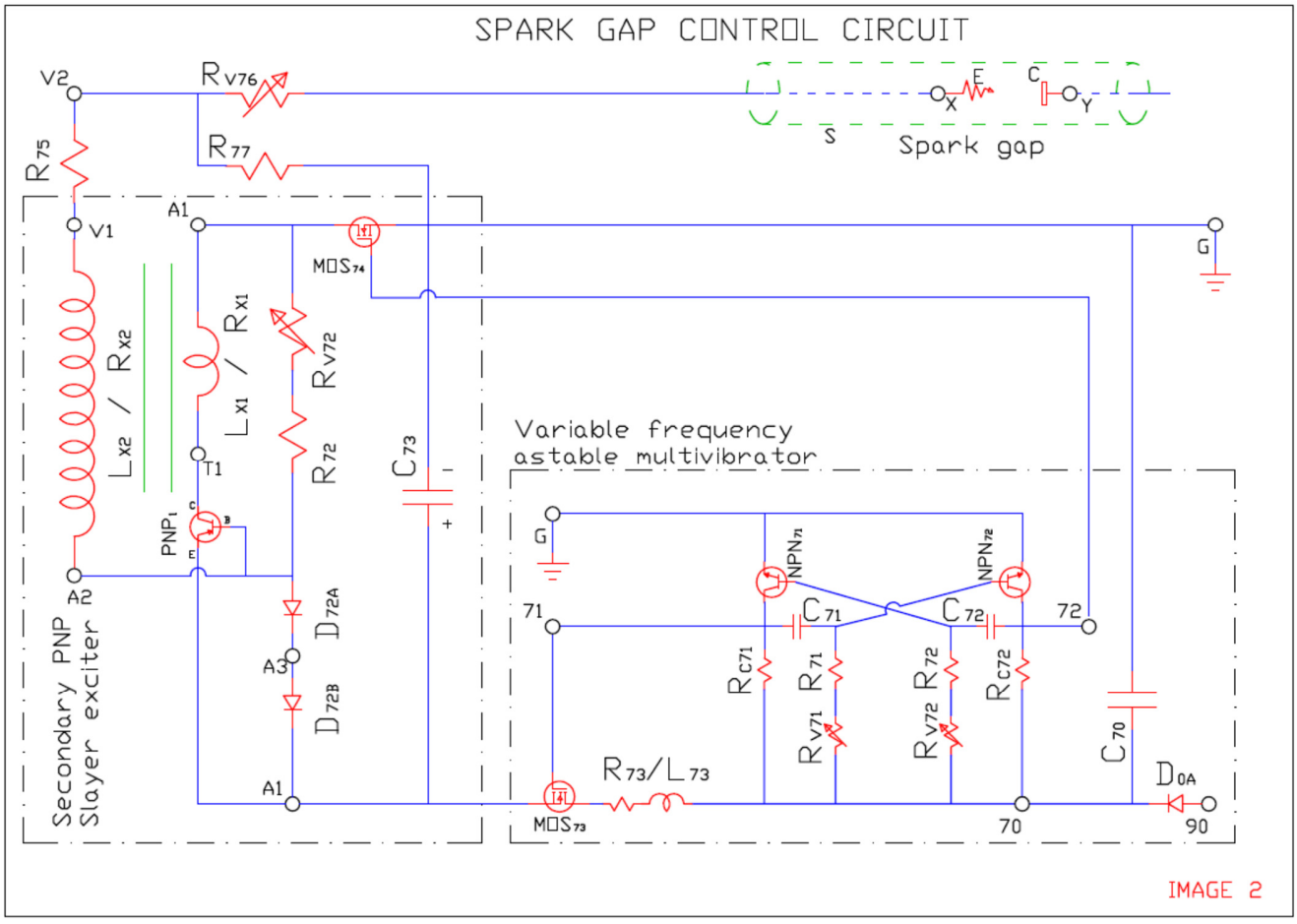
The emitter has a dedicated control circuit capable of accurately time the discharge frequency and duration of the spark (ie total electron quantity passing through the gap during each cycle).

In image 2 we have a variable frequency astable multivibrator feeding a PNP style slayer exciter which induces a negative voltage on the tip of the emitter E.

When the slayer exciter is disconnected from its power source (super condenser C73) a counter voltage (positive this time) is induced on tip E thus stopping the flow of electrons emitted until the next spark cycle begins.

The purpose of this control is to prevent the formation of a stable arc (short circuit) across the spark gap, maximize terminal electron velocity on the collector side of the gap and at the same

time minimize the discharge of the high (positive) voltage side of the circuit (node Y), thus minimizing energy requirement of the main NPN slayer exciter.



ON OFF controls

The slayer exciter has a spring return normally open switch S0 (D0 red LED is ON), when the red LED is ON it means the starter battery is powering the spark gap circuitry.

The operator needs to keep the button down for few seconds until supercondensers C3 and C4 are charged up to a level high enough to support operation of the slayer exciter without the aid of the battery (green LED is ON) meaning overrunity power supply is supporting the inverter

operation.

The energy recovery circuits

The energy recovery circuit 1 and 2 are ultimately going to furthermore increase their voltage V3 and V4 until also the load circuit is activated by automatic switch MOS-90 and net free energy power is made available through the load resistance.

The energy recovery circuit 1 tries to capture energy radiating from the collector when accelerated electrons impact with atoms of the metallic matrix and decay from local superluinar speed down to thermal speed. The pulsed radiation has been called also superelectric radiation or EMP radiation in previous papers and it is supposedly capable of displacing electrons off metallic materials like the spark gap metallic shield and through diode D3B, before fading and thus allowing electrons to be recalled back through diode D3A.
This pulsed current/voltage is stabilized by the supercondenser condenser C3 which could also undergo premature catastrophic failure because of said superelectric effect.

The second energy recovery circuit tests the possibility of magnetic monopole currents being generated during spark gap operation.
The inductor L4 is a wire coiled around the HV cable connecting to the spark gap collector or else an air core inductor with wire Y1-Y2 passing through its axis.

This inductor design is unprecedent in electronic applications since the magnetic current element $\vec{J}_B$ has always been neglected and set to ZERO within Maxwell equations but it is hereby assumed to be NON ZERO, hence the unusual design of inductor L4 which we shall call a Gray transformer to.

$$\oint \vec{E} \cdot d\vec{l} = \oiint_{\vec{S}} -\mu_0 \left(\vec{J}_B + \frac{1}{\mu_0} \frac{d\vec{B}}{dt} \right) d\vec{S}$$

The low voltage coil of the gray transformer L4 should generate a pulsed voltage between its terminals 4A and 4B, this voltage is stabilized by supercondenser C4 and net power is transferred to the load circuit through terminal 90.

Activation voltage for free energy effects to appear

As per discussion the electrons impacting on the collector must have a superluminar speed (in relation to the collector material speed of light) for superelectric effects to appear.

If we consider a collector made of iron (refraction index = 4) then the speed of light within the collector is 4 times lower than the speed of light in vacuum or else 75000 KM/sec.

This equals to 16000 Ev energy available for the electron crossing the gap or else translate in 0.53 CM minimum spark gap distance for superelectric effects to appear and be measured.

Controlling the power output

The load circuit features a variable resistor which directly controls the bus voltage of the system

(node 90 to Ground) as well as protecting the same from over voltages through safety MOS 91.

The higher the bus voltage the higher the power output through R Load as well as higher voltage induced between the spark gap terminals thanks to increased operating voltage (current) of the main slayer exciter.

Turning OFF the inverter

The most practical way to turn off the inverter is to turn off the HV generator powering the spark gap. A normally close spring return switch S1 has been added to achieve this feature.

To note that a failure on MOS 91 could lead to the system going into a runaway voltage increase until catastrophic failure of components MOS 90 and NPN1…

Additional control circuitry might be needed to furthermore protect the main and secondary slayer exciter circuits.